

Free Response: Write out complete answers to the following questions. Show your work.

- (10pts) 1. You have three resistors with specified resistances and uncertainties: $R_1 \pm \delta R_1$, $R_2 \pm \delta R_2$, and $R_3 \pm \delta R_3$.

10:10

(a) If the three resistors are connected in series, what is the equivalent resistance $R_s \pm \delta R_s$? Find expressions for R_s and δR_s in terms of R_1 , R_2 , R_3 and their uncertainties.

①

$$R_s = R_1 + R_2 + R_3 \quad \frac{\partial R_s}{\partial R_1} = 1 \quad \text{likewise for 2 \& 3}$$

②

$$\delta R_s = \sqrt{\delta R_1^2 + \delta R_2^2 + \delta R_3^2}$$

(b) If the three resistors are connected in parallel, what is the equivalent resistance $R_p \pm \delta R_p$? Find expressions for R_p and δR_p in terms of R_1 , R_2 , R_3 and their uncertainties.

①

$$R_p = \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \right)^{-1} \quad \frac{\partial R_p}{\partial R_1} = - \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \right)^{-2} \left(-\frac{1}{R_1^2} \right)$$

②

$$\delta R_p^2 = \frac{\delta R_1^2}{R_1^4} + \frac{\delta R_2^2}{R_2^4} + \frac{\delta R_3^2}{R_3^4} \\ \frac{\delta R_p^2}{\left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \right)^4}$$

(c) Suppose you want to make a 300Ω resistor. Given the limited equipment that you have in the lab, your options are to combine three $100 \Omega \pm 5\%$ resistors in series or to combine three $900 \Omega \pm 5\%$ resistors in parallel. Compare the resulting numerical values of δR_s and δR_p .

series : $R_1 = R_2 = R_3 = 100 \Omega \equiv R$

$$\delta R = (0.05)(100 \Omega) = 5 \Omega$$

$$\delta R_s = \sqrt{3 \delta R^2} = \sqrt{3} \delta R = 8.66 \Omega \quad (1)$$

parallel :

$$R_1 = R_2 = R_3 = 900 \Omega \equiv R$$

$$\delta R = (0.05)(900 \Omega) = 45 \Omega$$

$$\delta R_p^2 = \frac{3 \delta R^2}{R^4} = \frac{\delta R^2}{\left(\frac{3}{R}\right)^4}$$

$$\therefore \delta R_p = \frac{\delta R}{3^{3/2}} = \frac{45 \Omega}{3^{3/2}} = 8.66 \Omega$$

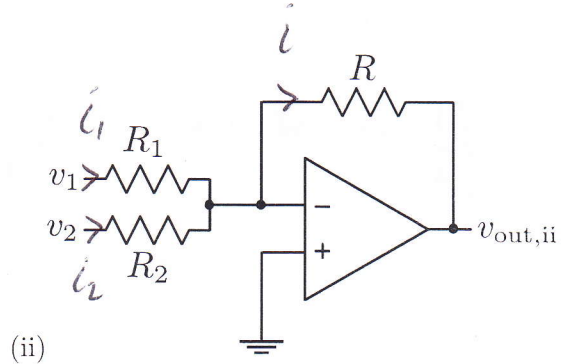
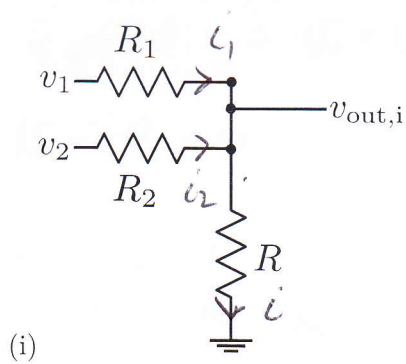
$$\boxed{\delta R_s = \delta R_p} \quad (2)$$

Both combination result in the same final ~~error~~ uncertainty $\delta R_{eq} = 8.66 \Omega$

Notice that the relative uncertainty $\frac{\delta R_{eq}}{R_{eq}} = 2.89\% < 5\%$!

0 pts

(10pts) 2. Consider the following two circuits:

(a) For circuit (i), find an expression for $v_{out,i}$ in terms of v_1 , v_2 , R_1 , R_2 , and R .

$$v_1 - i_1 R_1 = v_{out} \quad \therefore i_1 = \frac{v_1 - v_{out}}{R_1}$$

$$\text{likewise } i_2 = \frac{v_2 - v_{out}}{R_2}$$

$$i = i_1 + i_2 = \frac{v_1}{R_1} + \frac{v_2}{R_2} - v_{out} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

$$v_{out} = iR = \left(\frac{v_1}{R_1} + \frac{v_2}{R_2} \right) R - v_{out} \left(\frac{1}{R_1} + \frac{1}{R_2} \right) R$$

~~$$v_{out} \left[\frac{1}{R} + \frac{1}{R_1} + \frac{1}{R_2} \right] \therefore \frac{v_{out}}{R} = \left(\frac{v_1}{R_1} + \frac{v_2}{R_2} \right) - v_{out} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$~~

$$\therefore v_{out} \left(\frac{1}{R} + \frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{v_1}{R_1} + \frac{v_2}{R_2}$$

$$\therefore v_{out} = \frac{\frac{v_1}{R_1} + \frac{v_2}{R_2}}{\frac{1}{R} + \frac{1}{R_1} + \frac{1}{R_2}}$$

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(b) For circuit (ii), find an expression for $v_{out,ii}$ in terms of v_1 , v_2 , R_1 , R_2 , and R .

$$V_+ \text{ is grounded. } \therefore V_+ = V_- = 0$$

$$\therefore V_1 - i_1 R_1 = 0 \quad \therefore i_1 = \frac{V_1}{R_1} \quad \text{likewise } i_2 = \frac{V_2}{R_2}$$

$$i = i_1 + i_2 = \frac{V_1}{R_1} + \frac{V_2}{R_2}$$

$$0 - iR = V_{out}$$

$$\therefore - \left(\frac{V_1}{R_1} + \frac{V_2}{R_2} \right) R = V_{out}$$

(ii)

(c) Finally, in your expressions for $v_{out,i}$ and $v_{out,ii}$ from parts (a) and (b) set $R_1 = R$ and $R_2 = R$. Simplify your answers as much as possible and write down the resulting $v_{out,i}$ and $v_{out,ii}$ expressions.

$$\text{If } R_1 = R \quad R_2 = R$$

$$V_{out,i} = \frac{\frac{V_1 + V_2}{R}}{\frac{3}{R}} = \boxed{\frac{V_1 + V_2}{3}}$$

both summing circuits,
but (i) has $\frac{1}{3}$ factor
& (ii) is inverting.

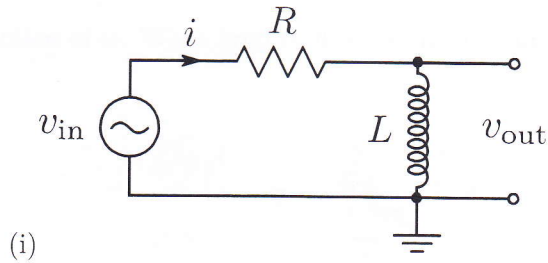
$$\text{If } R_1 = R \quad R_2 = R$$

$$V_{out,ii} = - \left(\frac{V_1 + V_2}{R} \right) R = \boxed{-(V_1 + V_2)}$$

(ii)

solns

(15pts) 3. Consider the LR-series circuit shown below:



(a) If the input voltage is given by $v_{in} = V_0 \sin \omega t$, what are the amplitude I_0 and phase ϕ of the current i ?

$$\textcircled{1} \quad I_0 = \frac{V_0}{|Z|} \quad \tan \phi = -\frac{\text{Im}[Z]}{\text{Re}[Z]} \quad \textcircled{1}$$

For R-L series combo

$$Z = R + j\omega L \quad \text{Im}[Z] = \omega L \quad \text{Re}[Z] = R$$

$$|Z|^2 = (R + j\omega L)(R - j\omega L) = R^2 + (\omega L)^2$$

$$\therefore |Z| = R \left(1 + \left(\frac{\omega L}{R} \right)^2 \right)^{1/2} = R \sqrt{1 + \left(\frac{\omega L}{R} \right)^2}$$

$$I_0 = \frac{V_0/R}{\sqrt{1 + \left(\frac{\omega L}{R} \right)^2}} \quad \textcircled{2}$$

$$\tan \phi = -\frac{\omega L}{R} \quad \textcircled{1}$$

Solutions

(b) For circuit (i) on the previous page, find an expression for $\left| \frac{v_{out}}{v_{in}} \right|$ in terms of ω , R , and L .

Sketch $\left| \frac{v_{out}}{v_{in}} \right|$ as a function of ω . What kind of filter is this circuit?

$$V_{in} = iZ \quad \therefore \frac{V_{out}}{V_{in}} = \frac{Z_L}{Z} \quad (1)$$

$$V_{out} = iZ_L$$

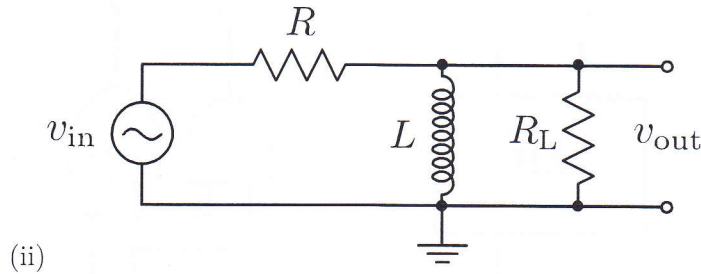
$$\therefore \left| \frac{V_{out}}{V_{in}} \right| = \frac{|Z_L|}{|Z|} = \frac{\omega L}{R \sqrt{1 + (\omega L/R)^2}} = \frac{\omega L/R}{\sqrt{1 + (\omega L/R)^2}} \quad (2)$$

$$\omega \rightarrow 0 \quad \left| \frac{V_{out}}{V_{in}} \right| \rightarrow \frac{0}{1} = 0$$

$$\omega \rightarrow \infty \quad \left| \frac{V_{out}}{V_{in}} \right| \rightarrow \frac{\omega L/R}{\omega L/R} = 1$$

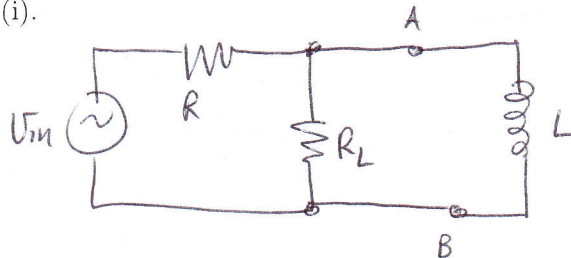


(c) If an oscilloscope is connected across the inductor, the input resistance R_L of the oscilloscope is placed in parallel with the inductor as shown below in circuit (ii):



For this modified circuit, what is the new expression for $\left| \frac{v_{out}}{v_{in}} \right|$? It is not necessary to do complicated calculations to find the appropriate expression. Instead, try coming up with an equivalent replacement that turns this back into a series circuit similar to the one shown in figure (i).

Redraw as

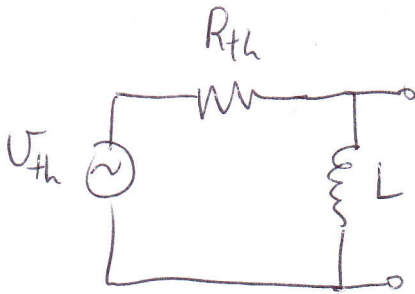


Replace everything to left of AB w/ Thevenin equiv.

$$V_{th} = V_{in} \frac{R_L}{R+R_L} \quad R_{th} = \frac{R R_L}{R+R_L}$$

→ voltage divider

$$\text{or } \frac{1}{R_{th}} = \frac{1}{R} + \frac{1}{R_L}$$



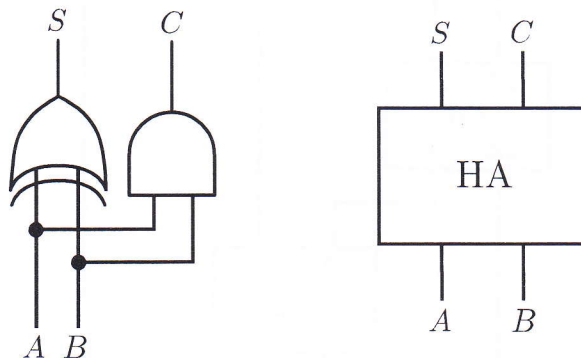
just like circuit (i)

$$\left| \frac{V_{out}}{V_{th}} \right| = \frac{\omega L / R_{th}}{\sqrt{1 + (\omega L / R_{th})^2}} \quad (2)$$

$$\therefore \left| \frac{V_{out}}{V_{in}} \right| \cdot \frac{1}{\left(\frac{R_L}{R+R_L} \right)} = \frac{\omega L \left(\frac{1}{R} + \frac{1}{R_L} \right)}{\sqrt{1 + \left[\omega L \left(\frac{1}{R} + \frac{1}{R_L} \right) \right]^2}}$$

$$\therefore \left| \frac{V_{out}}{V_{in}} \right| = \frac{R_L}{R+R_L} \frac{\omega L \left(\frac{1}{R} + \frac{1}{R_L} \right)}{\sqrt{1 + \left[\omega L \left(\frac{1}{R} + \frac{1}{R_L} \right) \right]^2}} \quad (3)$$

(10pts) 4. Recall the half-adder circuit used to add to single-bit binary numbers which has two inputs A and B and two outputs S and C :



(a) Write down the truth table for the half-adder circuit.

AND

X	Y	$X \cdot Y$
0	0	0
0	1	0
1	0	0
1	1	1

XOR

X	Y	$X \oplus Y$
0	0	0
0	1	1
1	0	1
1	1	0

(2.5)

Half Adder

A	B	S	C
0	0	0	0
0	1	1	0
1	0	1	0
1	1	0	1

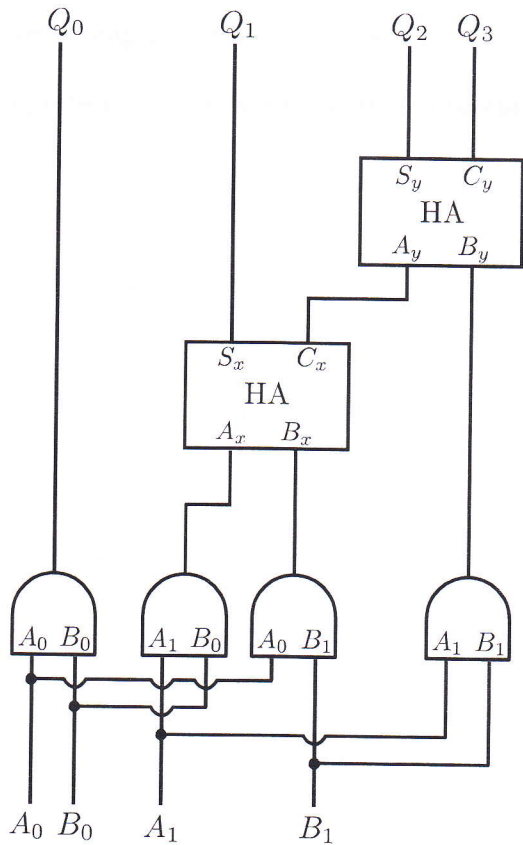
(b) Fill in the missing data on the truth table given on the next page. What kind of operation is this circuit performing on the pair of 2-bit binary inputs (A_1, A_0) and (B_1, B_0) ?

This circuit multiplies two 2-bit binary inputs $(A_1, A_0) \times (B_1, B_0)$.

(2.5)

sol'n's

- 0 0000
- 1 0001
- 2 0010
- 3 0011
- 4 0100
- 5 0101
- 6 0110
- 7 0111
- 8 1000
- 9 1001
- 10 1010



	A_1	A_0	B_1	B_0	A_x	B_x	S_x	C_x	A_y	B_y	S_y	C_y	Q_3	Q_2	Q_1	Q_0	
(0)(0)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(0)(1)	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
(0)(3)	0	0	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0
(2)(0)	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)(1)	0	1	0	1	0	0	0	0	0	0	0	0	0	0	0	1	1
(2)(2)	1	0	1	0	0	0	0	0	0	1	1	0	0	1	0	0	4
(3)(2)	1	1	1	0	0	1	1	0	0	1	1	0	0	1	1	0	6
(3)(3)	1	1	1	1	1	1	0	1	1	1	0	1	1	0	0	1	9

5

- (10pts) 5. Use Euler's equation ($e^{\pm j\phi} = \cos \phi \pm j \sin \phi$) to derive the following two trigonometric identities:

Note $e^{j\phi} + e^{-j\phi} = 2\cos\phi$

$$\therefore \cos\phi = \frac{e^{j\phi} + e^{-j\phi}}{2}$$

$$\begin{aligned} \therefore \cos^2\phi &= \frac{1}{4} (e^{j2\phi} + e^{-j2\phi} + 2) \\ &= \frac{1}{2} \left(\frac{e^{j2\phi} + e^{-j2\phi}}{2} + 1 \right) \end{aligned}$$

$$\therefore \cos^2\phi = \frac{1}{2} (1 + \cos 2\phi)$$

$$\cos^2\phi = \frac{1 + \cos 2\phi}{2}$$

$$\sin^2\phi = \frac{1 - \cos 2\phi}{2}$$

Note $e^{j\phi} - e^{-j\phi} = 2j\sin\phi$

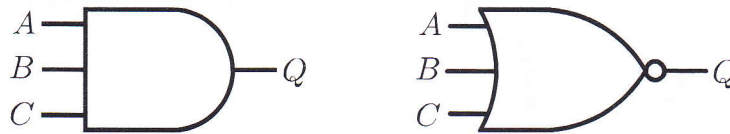
$$\therefore \sin\phi = \frac{e^{j\phi} - e^{-j\phi}}{2j}$$

$$\sin^2\phi = \frac{1}{4j^2} (e^{j2\phi} + e^{-j2\phi} - 2)$$

$$= \frac{1}{2} \left(1 - \left(\frac{e^{j2\phi} + e^{-j2\phi}}{2} \right) \right)$$

$$\therefore \sin^2\phi = \frac{1}{2} (1 - \cos 2\phi)$$

- (10pts) 6. In class we talked only about logic gates with only two inputs, however, it is possible to make some logic gates with any number of inputs. A 3-input gate AND and a 3-input NOR gate are shown below:



The truth for the 3-input AND gate is:

A	B	C	Q
0	0	0	0
0	0	1	0
0	1	0	0
0	1	1	0
1	0	0	0
1	0	1	0
1	1	0	0
1	1	1	1

- (a) Write down the truth table for the 3-input NOR gate.

For a 3-input OR gate
~~the~~ truth table would be

A	B	C	Q
0	0	0	0
0	0	1	1
0	1	0	1
0	1	1	1
1	0	0	1
1	0	1	1
1	1	0	1
1	1	1	1

3

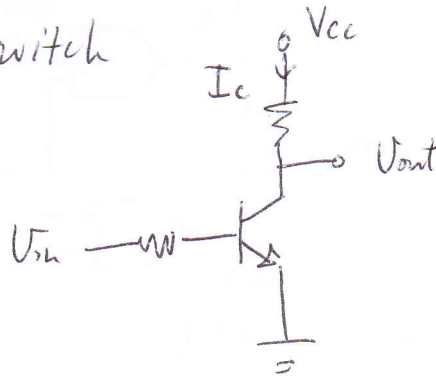
The 3-input NOR gate
is just the inverse output

A	B	C	Q
0	0	0	1
0	0	1	0
0	1	0	0
0	1	1	0
1	0	0	0
1	0	1	0
1	1	0	0
1	1	1	0

Sol'n's

(b) Design a 3-input NOR gate using only transistors and resistors. *Hint:* One common design uses three transistors.

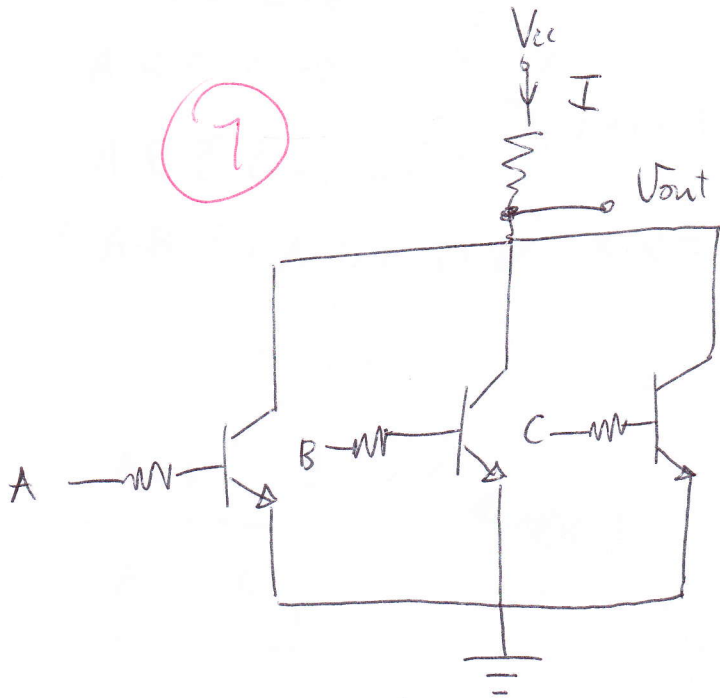
Recall ~~the~~ transistor switch



$V_{in} \text{ LO:}$
 $I_c \approx 0$
 $V_{out} = V_{cc} - I_c R$
 $= V_{cc}$
 $\therefore V_{out} \text{ is HI.}$

$V_{in} \text{ HI:}$
 $I_c \text{ large}$
 transistor forward biased
 $V_{out} \approx 0.2V \Rightarrow \text{LO.}$

Put transistor switches in parallel



I is large anytime one or more transistors conducting $\therefore V_{out} \rightarrow \text{LO}$
 $V_{out} \rightarrow \text{HI}$ only if all transistors in off state.

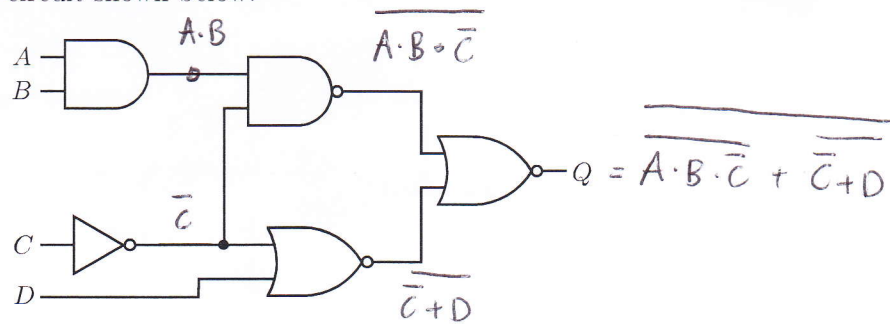
A	B	C	V_{out}
0	0	0	1
0	0	1	0
0	1	0	0
0	1	1	0
1	0	0	0
1	0	1	0
1	1	0	0
1	1	1	0



0pts

sol'n's

(10pts) 7. Consider the digital circuit shown below:



(a) Write down the logic expression for the output Q. (For example, recall that the logic expression for the X AND Y operation is $X \cdot Y$.)

$$Q = \overline{A \cdot B \cdot \bar{C} + \bar{C} + D} \quad (3)$$

(b) Simplify the expression for Q obtained in part (a) as much as possible. For part of your solution, you may find De Morgan's theorems helpful: $\overline{A \cdot B} = \bar{A} + \bar{B}$ and $\overline{\bar{A} + \bar{B}} = A \cdot B$. Draw the simplified digital circuit. Are any of the inputs irrelevant to the state of the output Q?

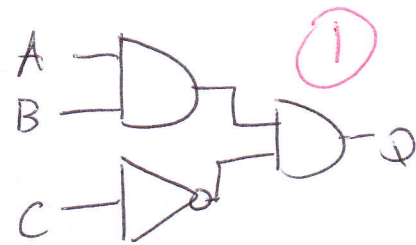
$$\begin{aligned}
 Q &= \overline{A \cdot B \cdot \bar{C} + \bar{C} + D} \\
 &= \overline{\overline{A \cdot B \cdot \bar{C}} \cdot \overline{\bar{C} + D}} \quad \text{DeMorgan} \\
 &= A \cdot B \cdot \bar{C} \cdot (\bar{C} + D) \quad \overline{\bar{X}} = X \\
 &= A \cdot B \cdot \bar{C} \cdot \bar{C} + A \cdot B \cdot \bar{C} \cdot D \quad \text{distributive} \\
 &= A \cdot B \cdot \bar{C} + A \cdot B \cdot \bar{C} \cdot D \quad X \cdot X = X \\
 &= A \cdot B \cdot \bar{C} \cdot (1 + D) \quad X \cdot 1 = X \\
 &= A \cdot B \cdot \bar{C} \cdot 1 \\
 &= A \cdot B \cdot \bar{C}
 \end{aligned}$$

$$Q = A \cdot B \cdot \bar{C}$$

~~AND OR~~

$$1 + X = 1$$

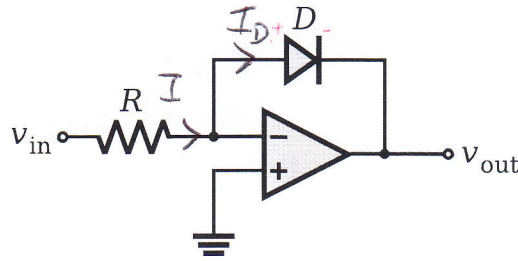
X	1	X+1
0	1	1
1	1	1



equivalent circuit.

Input D irrelevant to state of output Q. (1)

(10pts) 8. Consider the so-called "log amplifier" shown below:



Recall that the current in a diode is given by $I_D = I_0 (e^{eV_D/k_B T} - 1)$ where I_0 is a constant and V_D is the voltage across the diode. Assume that v_{in} and R are chosen such that $I_D \gg I_0$, show that:

$$v_{out} = G \ln \left(\frac{v_{in}}{RI_0} \right)$$

Find an expression for the proportionality constant G .

$$I_D = I_0 (e^{eV_D/k_B T} - 1) = I_0 e^{eV_D/k_B T} - I_0$$

if $I_D \gg I_0$, then $I_D \approx I_0 e^{eV_D/k_B T}$

V_+ grounded $\therefore V_+ = V_- = 0$.

$\therefore v_{in} - IR = 0 \quad \therefore I = \frac{v_{in}}{R}$

current into op amp is zero. $\therefore I = I_D$

$\therefore \frac{v_{in}}{R} \approx I_0 e^{eV_D/k_B T}$

Note also that $v_- - V_D = v_{out}$
 $\therefore v_{out} = -V_D$

→ Solve for V_D

$$\ln \left(\frac{v_{in}}{I_0 R} \right) = \frac{eV_D}{k_B T}$$

$\therefore V_D = \frac{k_B T}{e} \ln \left(\frac{v_{in}}{I_0 R} \right)$

$\therefore v_{out} = - \frac{k_B T}{e} \ln \left(\frac{v_{in}}{I_0 R} \right)$

$G = - \frac{k_B T}{e}$

$v_{out} \propto \ln v_{in}$
→ Log Amp.